A GUIDE TO TECHNICAL STANDARDS AND MEASUREMENTS FOR CABLE TELEVISION SYSTEMS



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This work is being published as a Technical Memorandum recognizing that the results are preliminary and for a limited audience. This work is being made available to other agencies planning to further develop standards and measurements for cable television.

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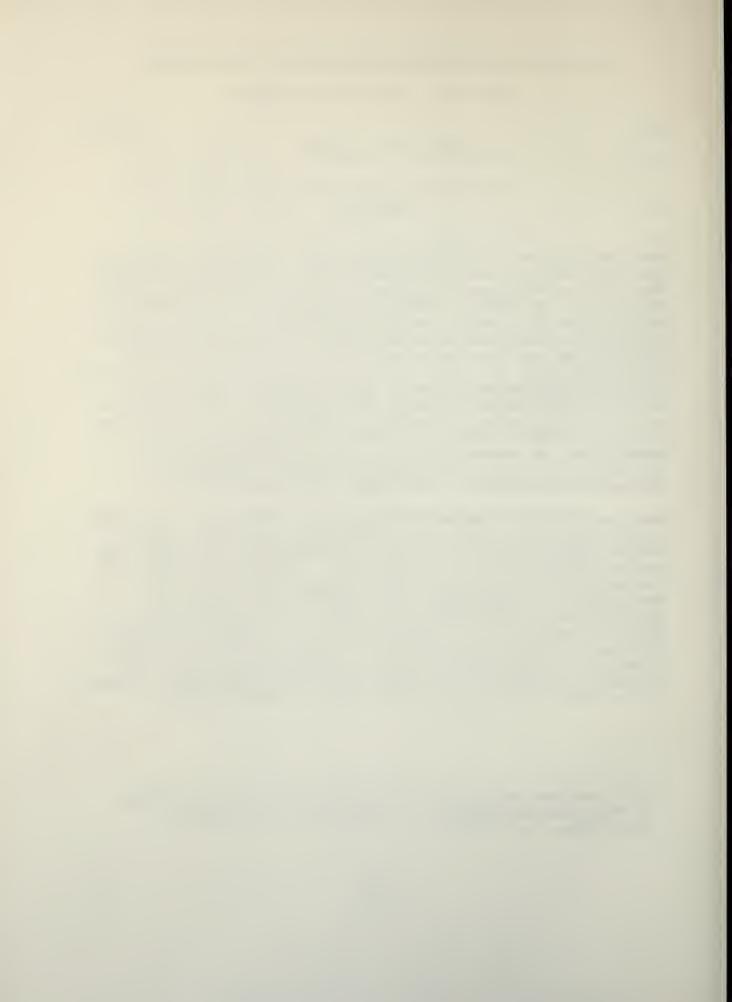
William C. Hsiao*

ABSTRACT

The preparation of this memorandum was supported in part by Grant No. SSH74-24664 from the National Science Foundation. The National Science Foundation awarded seven grants under Phase I of the program, "Design Studies for Experimental Application of Two-Way Cable Communications to Urban Social Service Delivery and Administration." The seven grantees provided to the Foundation on January 6, 1975, detailed final proposals for the execution of appropriate experiments in broadband communications. Under the NSF grant to the Office of Telecommunications, OT provided to the Foundation and the seven Phase I grantees technical advisory services, including draft versions of Sections 1 and 3 of this memorandum, to assure that the seven grantees had access to up-to-date technical information needed to adequately formulate and support their Phase II proposals.

Section 1 of the memorandum discusses CATV system technical requirements and lists referenced specifications, CATV system design criteria, system performance quidelines, and system construction specifications. Section 2 consists of ten measurement chapters which discuss test procedures applicable to measurement and evaluation of technical performance of CATV systems to assure compliance with the Federal Communications Commission's Rules and Regulations. Section 3 of the memorandum is a bibliography of technical literature concerned with cable television systems. The references have been organized into ten subject areas listed in the Table of Contents and consist of 807 entries.

^{*}This work was done while the author was with the Office of Telecommunications, U.S. Department of Commerce, Washington, D.C. 20230.



1. CATV SYSTEM TECHNICAL REQUIREMENTS

1.1 Introduction

It is vital to plan, construct, test, and operate any CATV system to the highest level of technical standards permissible by economical constraints and achievable within the framework of current technology. To meet this objective, the following system design criteria, performance guidelines, and construction suggestions have been developed.

Deviations from these guidelines may be required due to local conditions to conform to specific needs, problems, codes, etc., of its community. Therefore, the recommendations should be considered a general guideline rather than an inflexible set of rules.

1.2 Definitions

The following definitions shall apoly to terminology used in this guideline. Additional terms are defined in other portions of the guideline.

- Channel--Frequency spectrum of any information carrier.
- Distribution System--Any portion of the CATV system which contains cable, passive devices, hardware, or electronics which convey signals from the trunk caple to the subscriber drop cable.
- Trunk System--Any portion of the CATV system which contains cable, passive devices, hardware, or electronics which convey signals from the "head-end" to a distribution amplifier.
- Head-End--The electronic equipment located at the start of a cable system, usually including antennas, preamplifiers, heterodyne processing devices, frequency converters, modulators, demodulators, and other related equipment.

- Distribution Amolifier—Any amplifier used in the distribution system.
- Trunk Amplifier—Any amplifier used in the trunk system.
- Subscriber Drop--Output of subscriber tap-off device.
- Subscriber Drop Cable--Cable from subscriber drop to subscriber grounding block.
- Feeder Cable or Distribution Cable--Cable used in distribution system.
- Trunk Cable--Cable used in trunk system.
- Active Tap--A subscriber tap-off device which has active circuitry for providing amplification of signals to the subscriber drop.
- Set-top Converter--Electronic equipment used by each subscriber and placed before the television set which converts any or a block of the distributed television channels to a channel or channels on the television set.

1.3 Referenced Specifications

The following applicable documents are listed for reference.

- Federal Communications Commission (FCC) Rules and Regulations (R&R), Volume III, Parts 73 and 76.
- American National Standards Institute (ANSI) C1-1971.
- Electronic Industry Association (EIA) RS-170.
- National Cable Television Association (NCTA) Engineering Standards.
- National Electric Safety Code, National Bureau of Standards Handbook No. 130.
- Applicable Utility Joint Attachment Practices.

- City, County, and State Codes and Ordinances.
 - 1.4 CATV System Design Criteria (Refs. 231, 318, 402, 678, 680, 698, 707, 720)
- I. Coaxial Cable (Refs. 231, 707)
 - A. The following coaxial cable or its equivalent shall be used in the distribution system:
 - 1. 0.750 polyethylene foam cable with solid copper center conductor.
 - 2. 0.500 polyethylene foam cable with solid copper center conductor.
 - 3. 0.412 polyethylene foam cable with solid copper center conductor.
 - 4. 0.750 polystyrene foam cable with copperclad aluminum center conductor.
 - B. These cables shall be of solid aluminum sheath for aerial plant. Underground cable installations shall be protected by a high density polyethylene jacket and a viscous flooding compound.
 - C. Trunk and distribution coaxial cables shall have the following characteristics:
 - 1. Characteristic impedance of 75 ±2 ohms over the passband frequency range.
 - 2. High structural return loss, nominally 26 dB minimum in the frequency passband.

- 3. Maximum attenuation at 70 degrees F as follows:
 - a. 0.412" cable attenuation at 270 MHz = 1.87 dB/100 ft.
 - b. 0.500" cable attenuation at 270 MHz = 1.48 dB/100 ft.
 - c. 0.750" cable attenuation at 270 MHz = 1.10 dB/100 ft.
- 4. Maximum 60 Hz AC loop resistance at 70 degrees F as follows:
 - a. 0.412" cable--loop resistance of 2.4 ohms/1000 ft.

 - c. 0.750" cable--loop resistance of 0.7 ohms/1000 ft.
- D. Underground Cable—All underground cable shall adhere to the above specifications. In addition, where cable is installed in buried conduit, the cable shall contain an additional moisture barrier in the form of a flooding compound interspersed between the outer polyethylene jacket and the aluminum tubing. No trunk or distribution cable shall be directly buried unless it contains a protective steel outer covering (spiral wrap or corrugated), a second polyethylene jacket protecting the steel from corrosion, plus a moisture barrier flooding compound inside both the inner and outer jackets.
- E. Subscriber Drop Cables—In the case of dual cable system, overhead drop cables should preferably be dual type to present a neat appearance.

 Underground installations may be separate cables. However, in either case, 100 percent shielded type cable is required. Where a dual drop is installed underground, it should either be in plastic conduit or a cable type specifically designed for direct burial for the soil conditions indigenous to the area. In any event, direct burial drop cables should be preferably a dual jacket type with steel

outer wrap and moisture protective flooding compound.

II. Head-End Equipment (Refs. 706, 720)

- A. Antennas--Each antenna shall be of sufficient gain and directivity to provide adequate reserve of signal to noise ratio and suppression of adjacent channel interference. Co-channel interference levels shall be computed and each antenna selected and oriented for a theoretical minimum suppression of the undesired co-channel station. If necessary, the antenna height may be reduced to achieve required ratios. Except where specific needs dictate, all VHF antennas shall be of log periodic design. More than one station may be received on an individual antenna, providing all specifications can be achieved, including co-channel suppression. The following specifications shall apply:
 - 1. Antennas shall be ruggedized in construction with heavy duty cross arms and welded joints.
 - 2. All exposed metallic parts shall be adequately protected from corrosion.
- B. Converters and Preamplifiers--All active tower mounted devices shall be designed to operate continuously and meet full specifications under the most adverse weather and temperature conditions anticipated. Converters shall be frequency stabilized to conform to +25 kHz tolerance.
- C. Heterodyne Processing Devices--All processing amplifiers shall be solid state and of modular design. The following nominal specifications are given as a guideline.
 - 1. Response: +1 dB maximum over desired channel.
 - 2. Sensitivity: -20 dBmV input level for +55 dBmV output.
 - 3. Adjacent Carrier Rejection: 50 d3.
 - 4. Image Rejection: 60 dB.
 - 5. Output Level: Adjustable to +55 dBmV.

- 6. AGC Range: +0.5 dB output level variation for input levels of -20 dBmV to +20 dBmV.
- 7. Ambient Temperature Range: -20 degrees F to +100 degrees F.
- 8. Frequency Stability:
 - a. On channel: phase locked to TV station.
 - b. Off channel: +25 kHz of assigned frequency.
- D. Combining Network--The single channel head-end processing amplifier outputs shall be combined in a network which will result in maximum isolation between channels. The network should be designed so that a correct impedance match to each signal processed is maintained regardless of the condition of other processors in the system. High return loss, nominally 18 dB minimum, is desirable at all times at any input and output port of the network.

III. Trunk and Distribution Equipment (Refs. 231, 707)

- A. Equipment performance shall be such as to ensure that all specified system performance standards will be equaled or exceeded.
- B. All active circuitry in the equipment shall be transistorized.
- C. Lightning protectors shall be used in all active equipment to prevent damage due to induced lightning surges.
- D. All equipment shall be protected from accidental damage that could result from either short circuits or overvoltage. This protection shall be by fuses, circuit breakers, or other electrical devices.
- E. Outdoor equipments, except for AC power supplies, shall be housed in weatherproof, rugged, cast aluminum housing which are fully protected against corrosive elements of the region's atmosphere.
- F. All equipment shall be AC powered by a 60 dz waveform nominally 30 or 60 volts rms. This AC voltage could be multiplexed on the coaxial cable

or be brought directly into the trunk amplifier. AC power insertion will be made in a manner such that high isolation, nominally 50 dB, shall exist between the RF path and AC insertion point.

- G. Remote power supplies for powering of electronic equipment shall be ferro-resonant regulating, such that the AC voltage does not vary by more than +2% with an input voltage of 90 to 130 VAC.
- H. All active equipments (other than active taps) shall contain provision for directing AC power through the cable, selecting it from either an input and output port or directing it to either an input or output port.
- I. Test points shall be provided at inputs and outputs of trunk amplifiers and distribution amplifiers.

IV. Passive Devices (Refs. 707, 720)

- A. All passive equipment should be capable of having frequency response suitable for two-way operation. All taps shall be of the directional coupler type. Minimum isolation required between desired and undesired signal paths should be high, nominally 30 d3.
- B. Mechanically, the devices should be appropriately designed for the service intended application (i.e., indoor, outdoor, underground, etc.). Fittings should be mechanically and electrically secure, preferably of the center conductor screwdown type.
- C. Subscriber installation material such as cable fittings and grounding blocks should be a general good quality to provide firm and safe construction. Where grounding wire, rod, clamps, etc., are used, they shall be selected to conform to pertinent National Electric Code and local electrical safety specifications.
- D. Subscriber terminal 75 to 300 ohm balun shall have a low insertion loss, nominally 0.7 dB across the frequency passband.

- E. Cable A-B switches should be designed to electrically insert a terminating 75-ohm resistor or the output of the unused cable and provide a high degree of isolation, nominally 60 dB, between the desired and undesired cable signals.
- V. General System Design (Refs. 231, 380)
 - A. The RF System shall be designed to provide for distribution of a minimum of 20 television channels, where required, and additional FM broadcast signals. These television channels shall be contained in the standard television spectrum and in other available spectrum space within the frequency passband.
 - B. The FM broadcast signals will be carried in the standard FM frequency range of 88 to 108 MHz. These signals shall operate at nominally 15 dB below that of television channel six visual carrier.
 - C. Other information channels, such as data channels, AM broadcast channels, facsimile channels, etc., may be multiplexed in the transmission spectrum.
 - D. The System shall be rated for continuous 24-hour service in an environment of up to 100 percent humidity and of temperature variations from -20 degrees F to +100 degrees F.
- VI. Trunk System (Refs. 707, 720)
 - A. Spacing—Spacing between amplifiers shall be optional. A frequently used value is nominally 20 dB of cable as measured at 220 MHz at a cable temperature of 70 degrees F.
 - B. Signal Levels--Signal level shall be optional as long as the specified subscriber tap levels are maintained. A frequently used value is nominally 30 dBmV at 211.25 MHz. Tilt of other signals shall be optional.
 - C. Equalization--Each span of cable between amplifiers will be fully equalized in amplitude by the amplifier immediately succeeding the cable span so that cable attenuation and flat loss plus amplifier

gain equals unity at all frequencies in the passband.

D. Temperature Compensation

- Dual pilot carrier operation is preferred for automatic control of both level and slope under varying temperature.
- 2. One pilot carrier frequency shall be placed in the low end of the passband for level control. The other will be used in the high end of the passband for slop control.
- 3. Automatic level-control amplifiers shall operate such that, at their locations, pilot carrier drifts will be held to a mean of +0.5 dB nominally over the operating temperature.
- 4. Automatic level-control amplifiers will operate such that at -20 degrees F cross modulation of the trunk system will not be degraded below system performance requirements. At +100 degrees F, the automatic level control amplifiers will operate such that signal-to-noise ratio of any channel is not degraded below system performance requirements.
- 5. Automatic level-control amplifiers shall be used in sufficient quantities and spaced judiciously to maintain all system performance requirements under varying temperature.
- E. Trunk lines shall not be tapped for subscriber connection.
- F. All trunk cable shall be terminated with either matched electronic equipment or a termination of 75 ohms characteristic impedance.
- G. Splitting of trunk lines is permissible.

VII. Distribution System (Refs. 707, 720)

A. Output Levels--Bridger and line extender amplifier output levels and tilts are optional.

- B. Subscriber Tap Levels--The System shall be designed to provide a visual signal level on each channel of not less than one millivolt or 0 dBmV across an impedance of 75 ohms. Maximum output at any tap shall not be in excess of 10 millivolts or +20 dBmV across 75 ohms on any channel.
- C. All subscriber taps shall be of the directional coupler type with either 2, 4, or 3 output ports.
- D. Line extender amplifiers may be installed in cascade, as designed by system engineering considerations.
- E. All distribution cable will be terminated by a terminating multitap or by a termination of 75 ohms characteristic impedance.
- F. Splitting of distribution lines will be permitted.
- G. Equalization--All distribution cables between amplifiers will be properly equalized in amplitude so that amplifier gain plus cable loss, flat loss, and multitap loss equals unity at all frequencies in the passband.
- H. Distribution lines shall be isolated from trunk lines through either bridging amplifiers, distribution amplifiers, or other high isolation devices.
- I. Temperature Compensation
 - Automatic level control amplifiers shall be used so that at their locations, pilot carrier drifts will be held to +1.0 d3 nominally over the operating temperature range.
 - 2. Automatic level control amplifiers shall operate such that all prescribed subscriber tap levels shall be held to a maximum excursion of ±6.0 dB over the operating temperature range.
 - 3. Automatic level control amplifiers shall operate such that signal-to-noise ratio and cross modulation and intermodulation of the distribution system shall not be degraded below

system performance requirements over the operating temperature range.

1.5 System Performance Guidelines (Refs. 231, 318, 380, 402, 698, 706, 707, 720)

The following paragraphs describe the technical specifications for system performance regardless of location or distance. These performance parameters apply over the prescribed temperature operating range of the system from -20 degrees F to +100 degrees F. The specifications relate to factors affecting picture quality in the carriage of NTSC-TV signals within the standard 6 MHz bandwidth channels, as designated by FCC R&R, Section 73.682.

I. Head-End (Ref. 402, 698, 720)

This section covers performance of those portions of the system designed to process and transmit a single television channel (visual and aural) from the source (off-air or origination) to the multiplex combiner located at the distribution hub.

- A. Signal-to-Noise Ratio--This ratio of the head-end processing equipment is not specified separately, but included in the overall system specification.
- B. Channel Frequency Response--The channel frequency response shall be within a range of +2 dB for all frequencies within -1 MHz and +4 MHz of the visual carrier frequency.
- C. Video Modulation--Television channel modulators used either as part of the system or as test instruments shall be adjusted to 87.5% + 2.5% downward modulation at reference white level with FCC standard composite video waveform as indicated in FCC R&R, Section 73.699, Figure 6 or 7, as applicable.
- D. Transfer Linearity--Transfer linearity shall be adjusted for optimum practicable performance at 10 percent, 50 percent, and 90 percent of average picture level (APL). However, differential gain shall not exceed 2 dB, and differential phase shall

- not exceed 5 degrees for RF input, or 10 degrees for video input.
- E. Transient Response—Transient response to a 2T sine—squared pulse (T = 0.125 microseconds) shall fall within the limits indicated by a 5K rating. (Ref. 706)
- F. Chrominance Delay--Chrominance delay relative to luminance, as indicated by response to the modulated 20T pulse, shall not exceed +150 nanoseconds. Measurement accuracy shall be +20 nanoseconds or better.
- G. Low and Mid-Frequency Distortions--Low and midfrequency distortions, as indicated by response to the 60 Hz window signal, with a 2T transition, shall not exceed 5 IRE units in tilt, rounding, or overshoot. (Ref. 698, Section 73.682)
- H. Frequency of Visual Carriers—The frequency of each visual carrier shall be 1.25 + 0.025 MHz above the lower boundary of channel assignment.
- I. Frequency of Aural Carriers--The frequency of the aural carrier shall be 4 MHz +1 kHz above the frequency of the visual carrier.
- J. Center Frequency of FM Radio Carriers--The center frequency of all FM radio carriers shall be maintained within +10 kHz of the center.
- K. Best Engineering Effort—A best engineering effort shall be employed in antenna design, limited only by restrictions imposed by the state—of—the—art and zoning limitations, to avoid or to minimize co channel interference, electrical noise inter ference, multipath signals, or excessive fading.
- II. Distribution System (Refs. 231, 318, 698, 706, 707, 720)
 - A. Carrier-to-Noise Ratio (Refs. 698, 707, 712)
 - Definition--The ratio between the rms carrier voltage during sync interval to rms random noise voltage as measured or computed for a 4.0 MHz bandwidth receiver.

- 2. The carrier-to-noise ratio specification for any television channel in the passband is optional. The FCC limit is 36 dB minimum.
- B. Co-Channel Interference*--The ratio of visual signal level to any undesired co-channel television signal operating on proper offset assignment shall be optional. The FCC limit is 36 dB minimum.*
- *FCC requirements for performing tests to determine compliance with the standards of R&R, Section 76.605 (a) (9), insofar as it relates to the ratio of visual signal level to any undesired co-channel television signal, and Section 76.605 (a) (10), stating that the ratio of visual signal level to the rms amplitude of any coherent disturbances such as intermodulation products or discrete-frequency interfering signals not operating on proper offset assignments shall not be less than 46 dB, are hereby suspended for all cable television systems pending further action by the FCC.
- C. Cross Modulation (Refs. 698, 707, 714)
 - 1. Definition--Defined by NCTA Engineering Standard 002-0267.
 - 2. Specification for any television channel in the passband and over complete temperature range:
 - a. No visible evidence of cross modulation shall be noted at any point in the trunk or distribution system. Visible cross modulation is defined as presence of windshield-wiper effect on the television screen.
 - b. Cross modulation after any trunk amplifier shall be nominally -57 dB or less.
 Standards on permissible cross modulation have not been adopted by the FCC.
 - c. Cross modulation after any distribution amplifier shall be nominally -51 dB or less. Standards on permissible cross modulation have not been adopted by the FCC.

- D. Frequency Response (Refs. 698, 706, 707)
 - 1. Definition--The response, in dB, to a sweep frequency signal, expressed in peak-to-valley ratio in dB, where the peak and the valley are the maximum difference excursions of any frequency in passband, to that of the two end-points of the passband, when the two end-points are aligned on the sweep trace so that they are equal in level to each other.
 - 2. After "n" amplifiers of the trunk system, the peak-to-valley ratio of the frequency response shall be nominally (2 + n/12) d3.
 - 3. After any distribution amplifier the peak-to-valley ratio of the frequency response shall be nominally (2 + n/12 + 3) dB, where "n" is the number of trunk amplifiers in cascade before the distribution line.
 - 4. The peak-to-valley ratio of the frequency response over any 6 MHz channel at any point in the system shall be nominally less than 2 dB.
- E. The Visual Signal Level (Refs. 698, 707, 711)
 - Definition--Visual signal level is the rms voltage of a modulated television visual carrier across 75 ohms on a peak reading signal level meter, which is calibrated in rms voltage. For visual carriers this would be the carrier voltage during the sync interval.
 - Visual signal level on each channel within the passband at the subscriber terminals shall be a minimum of 1 millivolt or 0 dBmV across an impedance of 75 ohms, as required by FCC.
 - 3. The variation of visual signal level on each channel within any 24-hour period shall be a maximum of 12 dB, as required by FCC.
 - 4. The visual signal on each channel within the passband shall be maintained within the following FCC requirements:

- a. 3 dB of the visual signal level of any visual carrier within 6 MHz nominal frequency separation.
- b. 12 dB of the visual signal level on any other channel.
- c. A maximum level such that signal degradation due to overload in the subscriber's receiver does not occur.
- F. The Aural Signal--The rms voltage of the aural signal shall be maintained between 13 and 17 dB below the associated visual signal level, as required by the FCC.
- G. Intermodulation Distortion (Ref. 231, 698, 707)
 - 1. Definition--Intermodulation distortion is any spurious signal generated from either a second order, third order, or higher order beat signal between two or more carriers, or any harmonic generated from one carrier. This spurious signal appears as an interference signal in a channel of either the television or FM broadcast transmissions.

2. Specification

- a. No spurious signal shall be apparent as an interfering signal on the television picture of any of the television channel at any point in the trunk or distribution system.
- b. Any spurious interference signal generated as a result of intermodulation distortion shall be nominally at least 60 d3 down from the interfered channel carrier at any amplifier output in the trunk system.
- c. Any spurious interference signal generated as a result of intermodulation distortion shall be nominally at least 60 dB down from the interfered channel carrier at any point in the distribution system.

- H. Hum Modulation (Refs. 560, 698, 707)
 - 1. Definition--Hum modulation is the ratio between the level of a detected 60 Hz or 120 Hz signal from a carrier, compared to the detected signal from a 100 percent modulated carrier. Hum modulation is the ratio of one-half the peak-to-peak hum to the average carrier envelope. It can be expressed in decibels from 100 percent or in percentages.
 - Specification--The hum modulation shall be nominally less than 5 percent, as required by the FCC.
- I. Echo Distortion (Ref. 707)
 - Definition--Echo distortion is any reflected signal which appears as a trailing ghost in a television picture.
 - Specification—No trailing ghosts will be apparent on any television picture channel as viewed on a standard television receiver at any point in the trunk or distribution system.
- J. Direct Pick-up--Any direct pick-up causing leading ghosts or blanking bars shall not be visible on a thoroughly shielded test receiver or converter connected to any service drop. Ghosts, ringing, or reflections of any sort shall be eliminated, or minimized as much as possible, subject to limitations imposed by the technical state-of-the-art.
- K. Incidental Radiation (Refs. 534, 698)
 - Definition--Incidental radiation is the electromagnetic radiation in microvolts per meter from any point in the system, at any operating frequency, as measured by a standard dipole located at a proper distance from any point in the system.
 - 2. Specification--Incidental radiation from cable, amplifiers, connector hardware, passive devices shall not exceed the following limits:

- a. 15 microvolts per meter at a distance of 100 feet for frequencies up to and including 54 MHz.
- b. 20 microvolts per meter at a distance of 10 feet for frequencies over 54 up to and including 216 MHz.
- c. 15 microvolts per meter at a distance of 100 feet for frequencies over 216 MHz.
- L. Terminal Isolation—The terminal isolation provided each subscriber shall be a minimum of 18 dB as required by the FCC, but in any event, shall be sufficient to prevent reflections caused by open-circuited or short—circuited subscriber terminals from producing visible picture impairments at any other subscriber terminal.
- M. Dual Cable Switches--Where applicable, dual cable switches located at subscriber television terminals shall provide isolation between cables of at least 60 dB, and shall have a return loss of 16 dB or greater. No evidence of cross-coupling between the two cables shall be visible on any subscriber's television receiver.
- N. AC Primary Voltage Variation--All specifications shall be met for any primary supply voltage variation between 90 and 130 volts AC.
- O. Picture Quality
 - 1. Definition--The difference between a picture viewed on a standard television receiver as seen at the head-end and at the terminals of the distribution system.
 - 2. Specification--No television channel shall indicate additional presence of ghosting, hum bars, beat signals, cross modulation interferences other than that seen at head-end. Nor shall any color television picture indicate undue degradation of color fidelity and picture information at the distribution terminals.
- P. All relevant FCC technical performance rules shall be complied with.

- 1.6 System Construction Specifications (Refs. 318, 402, 678, 706, 707, 720)
- I. Construction Practices (Refs. 678, 720)
 - A. Installation and construction practices shall be in accordance with standard utility practice, utility company pole lease agreements, National Electrical Safety Code--Handbook No. 81, as amended by the latest edition, and state, city, and county ordinances.
 - B. All equipment shall be installed so as to be readily accessible for maintenance and shall be located so as not to interfere with the climbing space or servicing of other pole-mounted equipment. All strands shall be installed on the same side of the pole as the telephone facilities. Where telephone facilities do not exist, the strand shall be installed in the street side of the pole wherever possible.
- II. Anchors and Guys (Ref. 707)

The following guide shall be used for anchors and guys. The construction materials shall be used unless otherwise defined by pole lease agreements or any ordinances.

- A. The system shall be installed on 1/4" highstrength, seven wire, galvanized, zinc coating "A" supporting strand. The latter shall have a minimum breaking strength of 4,750 pounds.
- B. Where three or more consecutive spans exceed 250 feet in any given run, 1/4" extra high-strength, seven wire, galvanized, zinc coating "A" supporting strand, having a minimum breaking strength of 6,600 pounds shall be used.
- C. Supporting strand shall be placed at dead-end poles and corner poles where there is an angle of greater than 6 degrees.
- D. Anchors shall be 3/4" x 5', 6-inch screw type or 6-inch, 8-way expanding anchor with 5/8" x 6' rod.

- E. Guy strand size shall be the same as supporting strand unless otherwise specified.
- F. Guys shall be attached to standard pole line hard-ware and anchor rods using a preformed dead-end or strand vise. Where applicable, an auxiliary eye attachment will be used to attach the guy to an existing anchor rod.

III. System Bonding and Grounding (Refs. 678, 707)

- A. The CATV strand shall be bonded to telephone strand and/or other existing pole grounds in accordance with pole lease agreement, except there shall be a minimum bonding between parallel CATV and telephone strands at the first, last, and every tenth pole. Cable television plant shall be grounded at the latter locations.
- B. The CATV strand shall be grounded with No. 6 soft drawn bare copper wire at each power supply location using a 5/8" x 8' grounding rod, driven its full length plus 6 inches below the ground.

IV. Cable Installation (Ref. 707)

- A. The cable shall be lashed to supporting strand using 0.045 stainless lashing wire having an average of one wrap per linear foot of strand.
- B. At each pole and equipment location, the cable and strand shall be separated by use of cable supports and spacers. The lashing wire shall be terminated with a suitable change at each of these locations.
- C. Expansion loops shall be made at each pole and at each side of equipment and splice location to provide for expansion of cable caused by temperature variations.

V. Cable Pull-Out (Ref. 720)

All cables will have their center conductor and outer conductor properly seized at any splice or equipment entry so as to prevent cable pull-out due to temperature changes.

- VI. Splices and Connectors (Ref. 678)
 - A. Splices in trunk and feeder cable snall be properly sealed for water-proofing by placing silicone grease on the threads and "O" rings of the splice fittings. No waterproofing compound shall be allowed in the dielectric space.
 - E. Connectors to amplifiers and other devices shall be protected against moisture by placing silicone grease on threads and "O" rings of all fittings and tightening the fittings according to the manufacturer's specifications.

2. CATV SYSTEM TECHNICAL PERFORMANCE MEASUREMENTS

2.1 Introduction

This section discusses test procedures applicable to measurement and evaluation of technical performance of CATV systems (Refs. 508, 516, 527, 532, 551, 560, 582) to ascertain compliance with the Federal Communications Commission's performance tests and technical standards set forth under Subpart K of Part 76 of the Commission's Pules and Regulations (Refs. 696, 697).

It is not the intent of this section to outline the most elaborate techniques of measurement. The primary method, using equipment of reasonable cost, is described for each measurement of the various parameters. Where applicable, alternate methods and equipment are given for the measurement of several parameters. Models or manufacturers of test equipment are not specifically given. Pertinent information in this regard can be obtained from the National Cable Television Association, Washington, D.C.

In any measurement good engineering practices must be observed. In setting up test equipment all connecting cables and adaptors should be properly matched. It is desirable to use attenuator pads at connection points to minimize reflections due to mismatch. The proper impedance matching transformers or minimum loss matching pads must be used in interconnecting equipment of different impedance levels. The insertion loss of the matching devices, the signal attenuation of connecting coaxial cables, and the gain of any preamplifier must all be taken into consideration in the measurement result. The foregoing applies to all test procedures and is not redundantly repeated for each procedure.

Proper documentation of all measurements is essential. Test methods used, model and serial number of test equipment, and pertinent calibration information should be described. Sample forms for proper documentation and data recording are given in Pef. 55].

2.2 Frequency Measurements (Pefs. 487, 516, 551, 564)

I. Primary Method

A. Introduction

The frequency of a test signal is measured indirectly by the zero beat method. A substitute signal from a signal generator is tuned until its output frequency coincides with the test signal and is displayed by a frequency counter.

B. Test Equipment Required

- 1. Frequency counter.
- 2. RF signal generator.
- 3. Signal Level Meter (SLM).
- 4. Variable attenuator, 75-ohm impedance, 1-dB increment.
- 5. Two-way hybrid splitter, two each.
- 6. One pair of headphones.
- 7. Resistive terminator, 75 ohm.
- 8. (Optional) Spectrum analyzer or TV receiver.

C. Test Setup

Refer to Figure 1, page 2-27.

D. Test Procedure

- Set up the equipment as illustrated in Figure 1, page 2-27.
- Tune SLM for a peak reading of the test signal and record level.
- 3. Disconnect test signal input lead to splitter No. 2, which is then terminated with the 75-ohm terminator.

- 4. Adjust signal generator frequency and output level so as to obtain the same reading on SLM as recorded in step D2. (Note: The signal generator's full output may be required to give stable indication on some frequency counters. If so, the variable attenuator may be used to adjust the signal level fed into the SLM.)
- 5. Refer to step D3. Remove 75-ohm terminator. Reconnect test signal input lead to splitter No. 2. The SLM will now be receiving two signals of approximately the same frequency.
- 6. Adjust the signal generator's fine frequency vernier control carefully until the lowest frequency heterodyne (tone) can be heard on the headphones. (Note: When monitoring TV visual carriers, disregard the weak heterodyne, due to sidebands, appearing about 15 kHz above and below the main carrier. Use only the louder center frequency.)
- Read and record the frequency counter indication.
- 8. To measure TV aural carrier, the program modulation tends to obscure the heterodyne. Wait for a pause in the program. Then use the above procedure to obtain zero beat.
- 9. When measuring TV visual carrier, more precise frequency indication can be obtained by substituting a TV receiver in place of the SLM and headphones combination to obtain a true "zero" beat.

E. Optional Method

A spectrum analyzer, if available, may be used in place of the SLM and headphones to indicate frequency coincidence of the test signal and the signal generator. While the spectrum analyzer is more convenient, accuracy in the measurement depends upon the residual FM of the analyzer and how accurately the frequency coincidence is made.

II. Alternate Method

A. Introduction

The tracking generator is a special signal source whose RF output frequency tracks (follows) some other signal beyond the tracking generator itself. In conjunction with the spectrum analyzer, the tracking generator produces a signal whose frequency precisely tracks the spectrum analyzer tuning and can be indicated by a counter.

B. Test Equipment Required

- 1. Spectrum analyzer.
- 2. Tracking generator.
- 3. Frequency counter.

C. Test Setup

Refer to Figure 2, page 2-27.

D. Test Procedure

- 1. Set up the equipment as illustrated in Figure 2, page 2-27.
- 2. The spectrum analyzer/tracking generator system is used in the open-loop configuration.
- 3. The test signal is connected to the spectrum analyzer input.
- 4. The tracking generator output is connected to a frequency counter.
- 5. The spectrum analyzer is manually scanned to the test signal.
- 6. The counter displays frequency of the test signal.

E. Optional Method

The signal processor is capable of stripping modulation and producing a direct output for a

frequency counter. When measuring TV visual and aural carriers within its range, the signal processor can be used to receive the test signal. The processor's output is fed to a counter for readout.

2.3 Visual and Aural Signal Levels (Refs. 516, 535, 551)

I. Primary Method

A. Introduction

Measurement of the visual and aural signal levels can be made directly from the spectrum analyzer. For greater accuracy the signal levels are measured one at a time by comparing the amplitude of each signal with the output from a calibrated signal generator on a spectrum analyzer. The measurement can be repeated at regular intervals for a consecutive 24-hour period, if required.

- B. Test Equipment Required
 - 1. Calibrated signal generator.
 - 2. Spectrum analyzer.
- C. Test Setup

Refer to Figure 3, page 2-28.

- D. Test Procedure
 - 1. Set up the equipment as illustrated in Figure 3, page 2-28.
 - 2. Tune the spectrum analyzer for a maximum displayed amplitude of the test signal.
 - 3. Center the display and use the analyzer reference level control to bring the signal level to the top graticule line of the CRT. (Note: When measuring visual signal, it is necessary to use a wide enough resolution

bandwidth of the analyzer to obtain sufficient spectral components. Typically, a 100 kHz bandwidth is required to read the peak value of the carrier in terms of rms volts with the modulation on. A narrower bandwidth would show a lower than actual level.)

- 4. Use the calibrated signal generator as a substitute device in place of the test signal. Adjust the signal generator's frequency and output level controls to duplicate the result of step D3, in order to verify the amplitude accuracy.
- 5. Read the generator output level and record the result as the desired signal level.
- 6. If a calibrated signal generator is not available, calibrate the spectrum analyzer using its internal calibrator. The signal level will then be given by the analyzer Peference Level setting. The accuracy will be a function of the analyzer's internal calibrator accuracy, the flatness of the analyzer, and the Peference Level accuracy.

II. Alternate Method

A. Introduction

A conventional signal level meter may be used for the measurement of visual and aural signals, if a spectrum analyzer is not available. Make certain that the signal level meter is in good working order and has been calibrated prior to usage.

B. Test Equipment Required

Signal level meter.

- C. Test Procedure
 - 1. Connect test signal to the signal level meter.
 - 2. Tune signal level meter for a beak reading of the test signal.

 Measure and record all visual and aural signal levels.

2.4 Hum Measurements (Refs. 493, 516, 551)

I. Primary Method

A. Introduction

Hum modulation of visual carriers can show up on the TV receiver as horizontal bars that move slowly up or down. Due to the close spacing of the modulation sidebands to the carrier, typically 60 or 120 hertz, frequency domain examination of low modulation percentage is difficult. Modulation of this type is conveniently measured in the time domain. An unmodulated carrier is tuned and detected by a spectrum analyzer used in the zero scan time domain mode. The analyzer's video output is then fed to an oscilloscope to observe and measure the ac hum.

B. Test Equipment Required

- 1. Spectrum analyzer
- 2. Oscilloscope.
- RF signal generator.

C. Test Setup

Refer to Figure 4, page 2-28.

- 1. Set up the equipment as illustrated in Figure 4, page 2-28.
- 2. The test signal should be unmodulated. When measuring visual carrier substitute an unmodulated carrier of the same frequency and amplitude from the signal generator.

- 3. Connect the analyzer's video output to the oscilloscope vertical input with a shielded lead. To minimize stray hum loops, make sure that there is no other ground on the oscilloscope case. If the oscilloscope has a three-pin power plug, use a two-pin adapter which has no ground pin. Synchronize the oscilloscope to the "line" at a frequency of 30 or 60 hertz.
- 4. The analyzer is used in the zero scan time domain mode as a filter and detector. The resolution bandwidth should be set to 30 kHz. Tune the analyzer to the desired unmodulated carrier.
- 5. Place oscilloscope in direct-coupled mode.
 Adjust scope gain and centering so that, with
 the signal source disconnected temporarily, the
 trace is on the bottom line of the scope screen
 and, with the signal source reconnected, the
 trace is in view and goes to a convenient line.
 Measure and record the dc voltage for later
 computation.
- 6. Switch the oscilloscope to ac coupling and center the trace vertically. Increase vertical gain of the scope sufficiently to measure and record the peak-to-peak ac voltage for later computation.
- 7. Hum modulation is usually symmetrical, varying both above and below the unmodulated level. Percent modulation is given by the formula:

percent modulation = 100 (E $_{max}$ - E)/(E + E) or

where (p-p variation) is the ac voltage measured
in step D6, where (ave. level) is the dc voltage

measured in step D5.

8. Measurement accuracy can be improved in the presence of noise by integrating the noise.

presence of noise by integrating the noise.
This is done by shunting the vertical input of
the oscilloscope with a capacitor chosen to have
no effect on the amplitude of the ac component.

II. Alternate Method

If a spectrum analyzer is not available, a conventional signal level meter may be used for the hum measurements. The use of a battery powered signal level meter is recommended to prevent any power line "ripple" from being introduced into the measurement. The test procedure is essentially the same as outlined in the primary method of 2.4 I, with the exception that the spectrum analyzer is replaced by the signal level meter.

2.5 Channel Frequency Response (Refs. 516, 551, 582)

I. Primary Method

A. Introduction

The individual channel frequency response is checked from at least 1 MHz below the visual carrier to 4 MHz above. The test is done in two parts. First, the CATV distribution system response is determined. Then the single channel signal processing equipment at the head-end is separately measured. The results of the two parts are combined to yield the overall measurement. A simultaneous sweep system is used for the test without removing TV channel from service.

B. Test Equipment Required

- 1. Simultaneous sweep transmitter.
- 2. Simultaneous sweep receiver.
- Marker generator.
- 4. Signal level meter.
- 5. TV receiver.
- 6. Camera.

C. Test Setup

Refer to Figure 5, page 2-28.

D. Test Procedure

- 1. Set up the simultaneous sweep transmitter in the CATV system head-end. Usually, the sweeper can be inserted through a directional coupler ahead of the system output test point.
- 2. Adjust sweep output level 10 to 15 dB above the channel visual carrier level. Establish the output level in the CW mode, monitoring with signal level meter on the output test point.
- 3. Set up the sweeper for a 2-millisecond sweep rate and select a 5- to 20-second repetition rate. Adjust the sweep bandwidth to cover the desired frequency range, using the marker generator to define channel boundary.
- 4. Observe the test channel on the TV receiver to verify that interference from the simultaneous sweep system is negligible.
- 5. Mark trace of the reference level on the sweep receiver. Using the sweeper's built-in step attenuators, marke traces higher or lower than the reference level in desired decibel steps for further reference.
- 6. Bring simultaneous sweep receiver to selected test site. Connect test signal to the sweep receiver. Observe and photograph response curve. Measure channel frequency flatness using reference traces established in setp D5.
- 7. Return to head-end. Determine frequency response of single channel signal processing equipment.
- 8. Combine results of steps D6 and D7 for overall channel frequency response.

II. Alternate Method

A. Introduction

If a simultaneous sweep system is not available, a manual point-by-point method of channel frequency response testing can be done by using a CW signal

generator at the head-end and a signal level meter at the test location. However, radio or telephone communication between the head-end and test location is required.

- B. Test Equipment Required
 - RF signal generator.
 - Signal level meter.
- C. Test Setup

Refer to Figure 6, page 2-29.

- D. Test Procedure
 - Measure the output level of the signal processor for the channel under test at the head-end with the signal level meter.
 - 2. Switch the signal processor to manual mode of operation. Set manual gain to give the same output level as measured in step D1. If applicable, disable the internal substitution carrier of the signal processor.
 - 3. Remove antenna feed for the channel under test and connect the signal generator in its place.
 - 4. Adjust signal generator frequency and output level so that the signal processor output level is the same as measured in step D1.
 - 5. At the test location of the system, this signal is measured with the signal level meter.
 - 6. The signal generator frequency is changed in desired increments, such as 0.5 MHz, to cover the required range of one MHz below the visual carrier frequency to four MHz above. For each frequency setting, make sure that signal generator output has not changed. Measure and record the signal level for each frequency.

2.6 Carrier-to-Noise Measurements (Refs. 514, 551, 560)

I. Primary Method

A. Introduction

The noise level in each channel is measured with a spectrum analyzer. The displayed noise level reads low due to two factors. First, the analyzer resolution bandwidth is to be normalized to the required 4 MHz, since noise power is proportional to bandwidth. The second factor is due to the log shaping and detector characteristics of the analyzer. The corrected noise level will be compared to the visual carrier level to obtain the carrier to noise ratio.

B. Test Equipment Required

- Spectrum analyzer.
- 2. Tunable bandpass filter, 6 MHz bandwidth.

C. Test Setup

Refer to Figure 7, page 2-29.

- 1. The test signal is connected through a tunable bandpass filter to the spectrum analyzer.
- 2. Tune both the filter and analyzer to the channel under test for a maximum displayed amplitude of the visual carrier. Use a 100 kHz resolution bandwidth on the analyzer, but the video filter is not used.
- Use the reference level control of the analyzer to place this signal on the top graticule line of the CRT.
- 4. Tune the bandpass filter slightly to insure that the noise in the spectrum between the visual carrier and color burst is a maximum. Change the analyzer resolution bandwidth to 10 kHz.

Use sufficient video filtering to smooth out the noise display. The sweep speed of the analyzer should be slowed down to avoid "sweep rate errors."

- 5. The displayed noise level should be measured directly from the analyzer screen to ascertain the number of decibels down from the top graticule line.
- 6. The displayed noise level is to be increased by the appropriate correction factor recommended by the analyzer manufacturer. Subtract this correction in decibels from the number of decibels obtained in step D5 to give the carrier-to-noise ratio.

II. Alternate Method

A. Introduction

If a spectrum analyzer is not available, the conventional signal level meter, with suitable correction, can be used for the measurement of carrier-to-noise ratio. Noise indication of the signal level meter is to be corrected upward due to normalizing of the IF bandwidth to 4 MHz. A second correction is in the opposite direction, because the peak detector commonly used by signal level meter gives higher noise reading. (Noise has a higher peak to RMS ratio than CW signals. As the detector output is reduced, its efficiency is lowered and reads closer to RMS value.)

B. Test Equipment Required

- 1. Signal level meter (SLM).
- Variable attenuator, 75 ohm, range of 60 dB, in 1 dB steps.
- 3. Tunable bandpass filter, 6 MHz bandwidth.
- 4. Resistive terminator, 75 ohm.

C. Test Setup

Refer to Figure 8, page 2-29.

- Set up equipment as illustrated in Figure 8, page 2-29.
- 2. Switch in 60 dB of attenuation in variable attenuator.
- 3. Place signal level meter on its most sensitive range.
- 4. Tune the SLM to a peak reading at the center of visual carrier for the test channel. Adjust variable attenuator setting, SLM compensator setting, and/or SLM meter range to give a convenient reference reading, such as center scale, on the SLM.
- 5. At the head-end, adjust the signal processor for the test channel to manual mode of operation. Set manual controls for normal operating level. Remove antenna input lead form signal processor, and substitute a 75-ohm terminator in its place. (Disable substitute carrier generator in signal processor, if applicable.)
- 6. Tune the SLM carefully across the test channel for minimum noise reading. Remove attenuation from the variable attenuator until the same reference reading of step D4 is obtained. Record the amount of attenuation in decibels removed.
- 7. The SLM's indicated noise level is to be increased by the appropriate correction factor. (This correction factor may be determined by having the SLM calibrated on a known noise source. Otherwise, use the average correction recommended by the SLM manufacturer.) Subtract this correction in decibels from the number of decibels obtained in step D6 for the carrier-to-noise ratio.
- 8. For greater noise measurement accuracy, it is desirable that all carriers be removed from the system except the pilot carriers required for automatic gain and/or slope controls.

2.7 Co-Channel Interference Measurements (Refs. 486, 516, 551)

I. Primary Method

A. Introduction

Offset co-channel interference is measured with a calibrated spectrum analyzer of adequate selectivity. The test channel signal is fed to an analyzer through a tunable bandpass filter. The filter is used to prevent the possibility of the analyzer contributing any distortion to the measurement. The amplitudes of the desired visual carrier and co-channel interference, if any, are displayed on the analyzer for direct comparison.

B. Test Equipment Required

- 1. Spectrum Analyzer.
- 2. Tunable bandpass filter, 6 MHz bandwidth.

C. Test Setup

Refer to Figure 7, page 2-29.

- 1. The test signal is connected to the spectrum analyzer through a tunable bandpass filter.
- Tune both the filter and the analyzer to the channel under test for a maximum displayed amplitude of the visual carrier.
- 3. Reduce frequency scan of the analyzer to 10 kHz per division with a resolution bandwidth of 1 kHz or less. Maximum video filtering should be used so that the video information will not obscure the display.
- 4. Center the visual carrier display. If cochannel interference is present, it will appear as an additional carrier in a position 10 or 20 kHz either side of the visual carrier.

- 5. Measure and record the level of co-channel interference relative to the visual carrier.
- 6. For greater accuracy, set the visual carrier level at the reference level on the CRT, and read the reference level setting. Then use the reference level control to bring the interference product to the top of the CRT. Subtract these two reference level settings to get the ratio of the visual carrier signal to the cochannel interference.

II. Alternate Method

An approximate method may be used if a spectrum analyzer is unavailable. This method consists of visually examining the test channel (Channel A) on a TV screen for possible offset co-channel interference as indicated by "venetian blind" effect. If such interference is observed, its level may be determined roughly by the use of a substitution oscillator. Tune the oscillator to simulate the observed co-channel beat on another TV channel free of interference (Channel B). Display both Channels A and B simultaneously on two TV receivers. The level and frequency of the substitute oscillator signal are finely adjusted to create a similar type of interference on Channel B as that observed on Channel A. The oscillator level may then be measured by a signal level meter to give the approximate value of co-channel interference.

2.8 Intermodulation Measurements (Refs. 493, 516, 527)

I. Primary Method

A. Introduction

Intermodulation is defined as the generation of sinusoidal components having frequencies equal to the sums and differences of integral multiples of the frequencies of the sinusoidal components introduced into the system. This occurs when the transfer characteristic of the system is nonlinear. Intermodulation distortion is measured with a calibrated

spectrum analyzer of adequate selectivity. The test channel is fed to an analyzer through a tunable bandpass filter. The amplitudes of the desired visual carrier and intermodulation products are displayed on the analyzer for direct comparison. This test may be performed with modulation on in the channel under test by using maximum video filtering to eliminate the video. However, since intermodulation components may be present coincident with one of the discrete sidebands, it is best to turn the modulation off.

- B. Test Equipment Required
 - 1. Spectrum Analyzer.
 - 2. Tunable bandpass filter, 6 MHz bandwidth.
 - 3. RF signal generator.
- C. Test Setup

Refer to Figure 7, page 2-29.

- D. Test Procedure
 - The test signal should be unmodulated. When testing a TV channel, replace the visual carrier with an unmodulated carrier of the same frequency and amplitude from the RF signal generator at the head-end.
 - 2. At the test location, the test signal is connected to the spectrum analyzer through a tunable bandpass filter. The filter is used to prevent the possibility of the analyzer contributing any distortion to the measurement.
 - 3. Tune both the bandpass filter and the analyzer to the channel under test for a maximum displayed amplitude of the unmodulated carrier.
 - 4. Set the unmodulated carrier level at the reference level on the analyzer CRT, and read the reference level setting.
 - 5. Scan the entire channel under test carefully for discrete interference products by varying the

analyzer scan, resolution bandwidth and sweep time controls.

- 6. Bring the interference product to the top of the analyzer CRT with the reference level control.

 Read the reference level setting.
- 7. Subtract the reference level setting obtained in step D6 from that of step D4 to give the ratio of the intermodulation interference ratio.
- 8. To insure that the analyzer is not contributing distortion, change the input attenuator of the analyzer by, say, 10 dB. If all signals change by exactly 10 dB, they are real spurious interference signals and not created by the spectrum analyzer.

2.9 Cross Modulation Measurements (Refs. 493, 560, 714)

I. Primary Method

A. Introduction

Cross modulation is the transfer or "crossing" of modulation from the interfering signal or signals to the desired signal. This occurs when the transfer characteristic of the system is nonlinear. CATV system, severe cross modulation results in a weak reproduction of the picture of the interfering channel superimposed on the picture being viewed. Since the receiver's horizontal scanning is synchronized with the wanted signal but usually not with the interfering one, the two horizontal frequencies usually differ slightly. Consequently, the interfering picture moves back and forth across the TV screen, producing slanting bars which give the so-called "windshield wiper" effect. equipment required to measure cross modulation will consist of a transmitting and a receiving package. The transmitting package is a multi-carrier signal generator unit whose output frequencies correspond to the TV channel assignments of the system being tested. The carriers are 100 percent modulated

synchronously by a symmetric square wave having a frequency of 15.75 kHz. The modulation of each carrier of the multi-carrier signal generator may be individually turned on or off, and the output level of each carrier may be adjusted separately. The receiving package consists of a signal level meter (SLM) and a narrow bandwidth wave analyzer. At the test location, the SLM is tuned to a CW carrier for the channel under test, while all other channels are 100 percent modulated. The video output of the SLM is connected to the wave analyzer, which is tuned to 15.75 kHz and has been calibrated for 100 percent modulation. Read cross modulation directly on the wave analyzer.

B. Test Equipment Required

- 1. Multicarrier signal generator unit.
- 2. Signal level meter (SLM).
- 3. Tunable bandpass filter, 6 MHz bandwidth.
- 4. Wave analyzer.
- 5. Variable attenuator, 75-ohm impedance, 1-dB increment.

C. Test Setup

Refer to Figure 9, page 2-30.

- 1. At the head-end of the CATV system replace all signals (except pilot carriers) with signals of the multi-carrier signal generator unit, whose output frequencies correspond to the frequencies of the system's visual carriers.
- 2. Adjust the level of each carrier to normal system operating level.
- 3. Turn off the modulation for the carrier of the channel under test. All other carriers are 100 percent modulated synchronously by a symmetric square wave having a frequency of 15.75 kHz.

- 4. At the test location, set up the equipment as illustrated in Figure 9, page 2-30.
- 5. Tune both the bandpass filter and the SLM for a peak reading of a modulated carrier, such as one for a channel adjacent to the channel under test.
- 6. Adjust the variable attenuator so that the SLM reads a signal level of +10 dBmV.
- 7. Connect the SLM's video output to the wave analyzer. Tune the wave analyzer for a peak reading at 15.75 kHz. Calibrate the wave analyzer for 100 percent modulation.
- 8. Repeat steps D5 to D7, but tune the bandpass filter and the SLM to the unmodulated carrier of the channel under test. Read the cross modulation directly on the wave analyzer.
 - 2.10 Terminal Isolation Measurements (Refs. 516, 535, 551)

I. Primary Method

A. Introduction

The procedure for measuring terminal isolation involves using a leveled sweep oscillator at one subscriber terminal to sweep slowly across the frequency band of interest, and the output observed with a spectrum analyzer at an adjacent subscriber terminal. Terminal isolation is dependent, to a great degree, on the use of proper terminations at all cable outlets.

B. Test Equipment Required

- 1. Spectrum analyzer.
- Sweep oscillator.

C. Test Setup

Refer to Figure 10, page 2-31.

D. Test Procedure

- Adjust controls of the sweep oscillator to sweep slowly across the frequency band of interest with a leveled output.
- 2. Measure the sweeper's output level on the spectrum analyzer by using the analyzer's reference level control to bring the trace to the top of the CRT. Note the reference level setting.
- 3. Remove CATV signals from the distribution leg to be tested. Backfeed the sweep oscillator to the system from a subscriber terminal location, or a simulated one.
- 4. At the adjacent subscriber terminal, set the analyzer to scan the same range of frequency using a 100 kHz or greater resolution bandwidth and a rapid sweep rate. Use variable persistence, if available, to print out the response on the CRT.
- 5. Use the reference level control to bring the response trace to the top of the CRT. Read the reference level setting. Subtract this setting from the output level of the sweeper as noted in step D2 to get the terminal isolation in decibels.

II. Alternate Method

A. Introduction

If a spectrum analyzer or sweep oscillator is not available, the terminal isolation may be measured in the following fashion. A signal from a RF signal generator is backfed into the system from one subscriber terminal. How much signal arriving at an adjacent subscriber terminal is measured with a signal level meter to determine the terminal isolation at a given frequency. The procedure is then repeated for other frequencies.

- B. Test Equipment Required
 - 1. RF signal generator.
 - 2. Signal level meter (SLM).
 - Variable attenuator, 75-ohm impedance, 1-dB increment.
- C. Test Setup

Refer to Figure 11, page 2-31.

- D. Test Procedure
 - 1. Remove CATV signals from the distribution leg to be tested.
 - Adjust RF signal generator controls to supply a high-level, say, +30 dBmV, signal of the desired frequency.
 - 3. Switch in a given amount, say, 25 dB, of attenuation in variable attenuator.
 - 4. Connect RF signal generator output through the variable attenuator to the SLM. Tune the SLM for a peak reading of the desired signal.
 - 5. Adjust variable attenuator setting, SLM compensator setting, and/or SLM meter range to give a convenient reference reading, such as center scale, on the SLM. Record both the variable attenuator setting and the SLM reading.
 - 6. Back-feed the signal generator output to the system from a subscriber terminal location, or a simulated one. Make sure that the generator's frequency and output level remain the same as those used in step D2.
 - 7. At the adjacent subscriber terminal, read the signal level with the SLM through the variable attenuator. The SLM compensator setting, and/or the SLM meter range, and the variable attenuator setting remain the same as those used in step D5.

8. Remove attenuation from the variable attenuator until the same reference reading of step D5 is obtained on the SLM. The amount of attenuation in decibels removed gives the terminal isolation at the selected frequency. The procedure outlined from steps D1 through D8 is repeated for other frequencies as desired.

2.11 Radiation Measurements (Refs. 526, 533, 534)

I. Primary Method

A. Introduction

A resonant dipole antenna is used to measure an unknown field strength which can be related to the voltage measured at the end of a properly terminated transmission line. A balanced to unbalanced transition, or balun, is needed to match the dipole with the unbalanced coaxial cable normally used to feed the signal to a measuring device, such as a spectrum analyzer or signal level meter, which is preceded by a broadband preamplifier to increase its sensitivity.

The antenna length required to resonate at a given frequency (independently of any dielectric effects) depends upon the ratio of the length of the conductor to its diameter. If the antenna is made of rod or tubing and is not loaded unduly near the ends by insulators, the following formula will give the required physical length of a half-wave antenna in inches:

Length (inches) = $(5905 \times k)/f(MHz)$

where k is a function of the ratio of the free-space half wavelength to the conductor diameter and f is the frequency in megahertz. For all practical purposes, the value of k may be taken to be 0.95. Then the physical length of a resonant half wavelength antenna is given as:

Length (inches) = (5610)/f(MHz)

When a 75-ohm, half-wave dipole antenna is exposed to an RF field, the rms voltage delivered to a 75-ohm load is:

V =(The square root of 75) x 5.58 x E/f

where V is the output voltage in microvolts rms, E is the field strength in microvolts per meter, and f is the signal frequency in megahertz.

Conversely, if the voltage is known, the field strength is given by:

E = (0.0207)(V)(f) for 75-ohm antenna.

Radiation from a CATV system is likely to be both complex and different for each case. Its measurement will be affected by many factors, such as local standing wave conditions; ambient signals; auto ignition and high-level urban noises; and the presence of reflections from other wires, the ground, and nearby vehicles and buildings. It is recommended that, whenever possible, measurements of radiation be made at locations free of interference, using frequencies free of strong, off-the-air signals. If radiation is detected, probe around and find the spot where the signal is strongest to verify the measurement.

B. Test Equipment Required

- 1. Resonant dipole antenna, 75 ohm.
- 2. Balanced to unbalanced balun, 75 ohm.
- 3. Broadband preamplifier.
- 4. RF signal generator.
- 5. Spectrum analyzer or signal level meter.

C. Test Setup

Refer to Figure 12, page 2-31.

D. Test Procedure

1. Adjust the physical length of the dipole antenna to be a resonant half wavelength for the frequency being tested in accordance with the formula discussed in the 2.11 Introduction:

Length (inches) = (5610)/f(MHz)

- 2. Adjust RF signal generator controls to supply a low-level signal, say, -30 dBmV, at the test frequency to the spectrum analyzer.
- After the analyzer has been tuned to a peak reading at the test frequency, it is disconnected.
- 4. Connect the dipole antenna through the balun and the broadband preamplifier to the analyzer.
- 5. Keeping the antenna at the required distance from the test object, probe for presence of signal at the test frequency as monitored by the analyzer which has been pretuned in step D3.
- 6. If radiation is detected, maintain the specified separation while hunting for the location where the signal is strongest.
- 7. Record the signal level displayed by the analyzer. Make corrections due to gain of the preamplifier, loss of connecting coaxial cable, and loss of balun, if any.
- 8. Calculate the field strength, E in microvolts per meter, from the corrected rms voltage, V in microvolts, at the test frequency, f in megahertz, by the formula discussed in the 2.11 Introduction:

 $E = (0.0207) \times (V) \times (f) \text{ for } 75\text{-ohm system.}$

9. Part 76, Subpart K, of the FCC Rules and Regulations governs the technical standards applicable to radiation from a cable television system. Section 76.605(a)(12) gives the radiation limit to be 15 microvolts per meter at a distance of 100 feet for frequencies up to and including

54 MHz, 20 microvolts per meter at a distance of 10 feet for frequencies over 54 up to and including 216 Mhz, and 15 microvolts per meter at a distance of 100 feet for frequencies over 216 MHz.

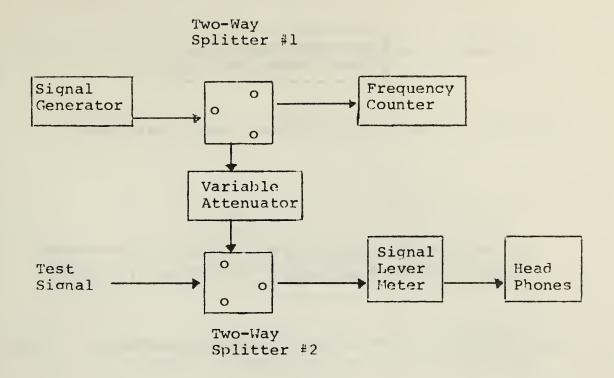


Figure 1. Test Setup for Frequency Measurements

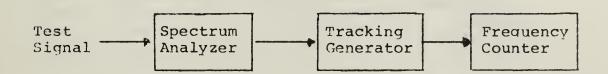


Figure 2. Test Setup for Frequency Measurements, Alternate Method

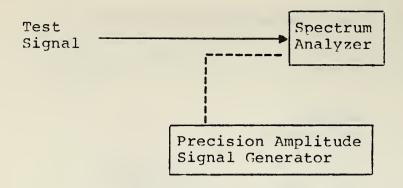


Figure 3. Test Setup for Signal Level Measurements

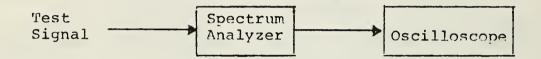


Figure 4. Test Setup for Hum Measurements

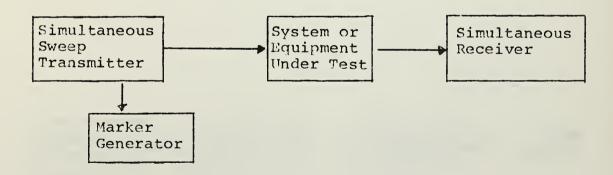


Figure 5. Test Setup for Channel Frequency Response

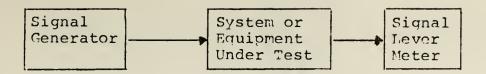


Figure 6. Test Setup for Channel Frequency Response, Alternate Method

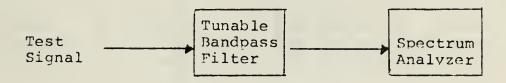


Figure 7. Test Setup for Measurements of Carrier to Noise, Co-Channel Interference, and Intermodulation

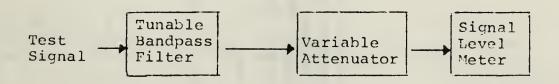
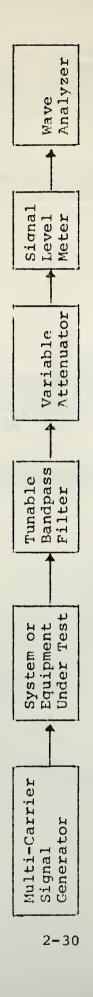


Figure 8. Test Setup for Carrier to Moise Measurements, Alternate Method



Test Setup for Cross Modulation Measurement Figure 9.

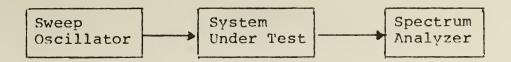


Figure 10. Test Setup for Terminal Isolation Measurement

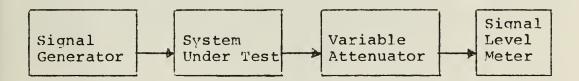


Figure 11. Test Setup for Terminal Isolation Measurement,
Alternate Method

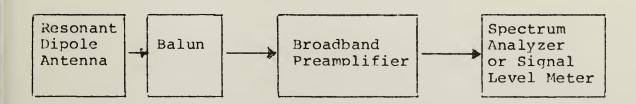


Figure 12. Test Setup for Radiation Measurements



3. BIBLIOGRAPHY

3.1 Introduction

This section consists of a bibliography of technical publications related to cable television systems. The reader is specifically referred to the seven-volume OT Report 73-13 entitled, "A Survey of Technical Requirements for Broadband Cable Teleservices," published by the Office of Telecommunications, U.S. Department of Commerce. Most of the technical references of OT Report 73-13 nave been selectively included in this section with the addition of up-to-date references. There are 307 references, which have been organized into ten subject areas listed in the Table of Contents. This organization is intended to aid in introducing the reader to specific subject areas.

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The preparation of this report was supported in part by Grant No. SSH74-24664 from the National Science Foundation. The National Science Foundation awarded seven grants under Phase I of the program, "Design Studies for Experimental Application of Two-Way Cable Communications to Urban Social Service Delivery and Administration." The seven grantees provided to the Foundation on January 6, 1975, detailed final proposals for the execution of appropriate experiments in broadband communications. Under the NSF grant to the Office of Telecommunications, OT provided to the Foundation and the seven Phase I grantees technical advisory services, including draft versions of Sections 1 and 3 of this report, to assure that the seven grantees had access to up-to-date technical information needed to adequately formulate and support their Phase II proposals. Section 1 of the report discusses CATV system technical requirements and lists referenced specifications, CATV system design criteria, system performance guidelines, and system construction specifications. Section 2 consists of ten				
measurement chapters which discuss test procedures applicable to measurement and evaluation of technical performance of CATV systems to assure compliance with the Federal Communications Commission's Rules and Regulations. Section 3 of the report is a bibliography of technical literature concerned with cable television systems. The references have been organized into ten subject areas listed in the Table of Contents and consist of 807 entries. 16.KEY WORDS (alphabetical order, separated by semicolons)				
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